

# Hygroscopic Behavior and Thermodynamic Properties of *Ziziphus joazeiro* Mart. Kernel Flour

Hanndson Araujo Silva (Corresponding Author), Josivanda Palmeira Gomes, Alexandre José de Melo Queiroz

Food Engineering Departament, Federal University of Campina Grande, Brazil

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#### Abstract

The hygroscopic and thermal behavior of kernel flour from *Ziziphus joazeiro* fruits were investigated. Adsorption isotherms were obtained at temperatures of 293, 303 and 313 K and adjusted to GAB, Oswin and Peleg models. The best fit of the experimental data was obtained with the GAB model with R<sup>2</sup> values> 0.994 and mean percentage deviation P < 10%. The isotherms obtained were sigmoidal type II. Isosteric heat and other thermodynamic properties were calculated as a function of moisture content. Adsorption isosteric heat decreased exponentially with increasing moisture content and differential entropy increased with moisture content, while differential enthalpy decreased. The theory of compensation confirmed that these properties are dependent on moisture content. The isotherms presented a spontaneous and enthalpy process.

Keywords: Hygroscopic behavior, thermodynamic properties, isosteric heat, Ziziphus joazeiro

# 1. Introduction

(*Ziziphus joazeiro* Mart), popularly known as juá, is a tropical fruit from the Rhamnaceae *Ziziphus* plant that is an endemic caatinga species mostly found on the northeastern Brazil (Brito et al., 2015).

Beyond the use for food, the local population uses the leaves, bark and roots for many other purposes comprising the production of traditional remedies for the treatment of several diseases (Brito et al., 2015). However, despite being a species widely used by the northeastern semiarid population, the exploitation of juazeiro is limited to extractivism (Silva et al., 2018).

For effective use and increasing the added value of seeds and grains, long term storage is essential (Lisboa et al., 2019). The moisture removal process is used to improve this shelf life



because the presence of moisture in kernel stimulates the development of microorganisms, causing irreversible damage and decreasing product quality (Avhad & Marchetti, 2016).

Knowledge of water sorption behavior becomes a necessary study to properly design drying equipment and processes. Using more accurate product drying procedures can prevent undesirable effects that may occur on the quality of the raw material. Sorption isotherms provide information on equilibrium moisture content (Xeq) and water activity (a<sub>w</sub>), simulating different relative humidity in equilibrium with the product (Polachini et al., 2016).

Liquid isosteric heat, enthalpy and differential entropy, and Gibbs free energy can be calculated from the sorption isotherms. These properties provide essential information about the sorption mechanism and drying process in terms of energy requirements (Aksil et al., 2019).

To date there is no research on the behavior of isotherms and thermodynamic properties of juá kernel reported in the literature. This fact justifies the study of their hygroscopic behavior aiming to provide information to prolong the shelf life of this unexploited product in the caatinga biome. Moreover, additional technological information can increase the uses and exploration of juá fruit. Therefore, the objective of this work was to describe the adsorption isotherms of juá kernels for different temperature conditions by evaluating the hygroscopic behavior and thermodynamic parameters by mathematical modeling, verifying the best fit to the experimental data.

# 2. Material and Methods

# 2.1 Raw Material

The fruits of juá (*Ziziphus joazeiro* Mart.) were collected in great state of maturity in *Ziziphus joazeiro* trees located at the Campina Grande campus of the Federal University of Campina Grande (UFCG)-PB.

# 2.2 Fruit Processing, Kernel Extraction and Flour Production

The fruits were previously washed in running water to remove impurities, then sanitized with chlorinated water for 15 min and rinsed with running water. Afterwards, the fruits were manually pulped, and from the residue generated by this processing the seeds were obtained. After these processes the seeds were broken to obtain the kernel and later stored in polyethylene packaging for use in the analyzes. Then the kernel were convectively dried at 343 K and afterwards were ground using a knife mill.

#### 2.3 Kernel Characterization

Freshly extracted and kernel flour were characterized for moisture content following the (AOAC method. 934.06, 2000). Lipid content was determined using chloroform and methanol (Bligh & Dyer method, 1959). Protein content was quantified by the Kjeldahl method with a conversion factor of 6.25 (AOAC method. 979.09, 2000). The ash content was determined by incinerating the samples in muffle furnace at 550 °C (AOAC method 923.03, 2000). Carbohydrate content was quantified by calculating the difference to 100%.



# 2.4 Adsorption Isotherms

Adsorption isotherms were determined by applying the static-indirect method at temperatures of 293, 303 and 313 K using the Decal Devices Aqualab Model 3TE water activity determinant (Crapiste & Rotstein, 1982). To set up a moisture-saturated environment, an airtight glass container filled with approximately 200 mL of distilled water was used. The vessel was placed in a constant temperature chamber and allowed to equilibrate moisture prior to each adsorption experiment. Approximately 1.5 g of flour was placed in a capsule and introduced into the container for the adsorption of water from the moisture saturated environment. At first, the sample was held for 5, 10, 20 and 30 min to adsorb moisture, and then intervals increased from 60 to 120 min for the last measurements. The methodology was repeated at 293, 303 and 313 K. After these time intervals, the sample was removed from the container, transferred to the water activity (a<sub>w</sub>) meter for measurement and then weighed on the scale. Then the sample was returned to the container to continue adsorbing moisture and the procedure was repeated until an a<sub>w</sub> value of about 0.9 was obtained.

# 2.5 Mathematical Modeling of Adsorption Isotherms

For the mathematical adjustment of the flour adsorption experimental data the Peleg, GAB and Oswin models were used (Table 1). The model parameters were determined by nonlinear regression using the Levenberg-Marquardt method in Statistica 12.0.

Model	Equation
PELEG	$Xeq = k_1 a_w^{n1} + k_2 a_w^{n2} $ (1)
GAB	$Xeq = \frac{x_m C k a_w}{(1 - k a_w)(1 - C k a_w)} $ (2)
	$(1 - k a_w)(1 - c - k a_w) $ (2) $C = C0 \exp\left(\frac{\Delta H m}{RT}\right) $ (3) $k = k0 \exp\left(\frac{\Delta H t c}{RT}\right) $ (4) $X_m = X_0 \exp\left(\frac{\Delta H_X}{RT}\right) $ (5)
	$\mathbf{k} = \mathbf{k}0 \exp\left(\frac{\Delta H t c}{RT}\right) \tag{4}$
	$X_m = X_0 \exp\left(\frac{\Delta H_X}{RT}\right) \tag{5}$
OSWIN	$Xeq = a \left(\frac{a_W}{(1-a_W)}\right) \tag{6}$

Table 1. Adjustment models of moisture adsorption isotherms.



Xeq – Equilibrium humidity (% dry basis);  $a_w$  – Water activity; Xm – Moisture in molecular monolayer; C e K – Parameters that depend on the temperature and nature of the product; a e b – Model fit parameters; k1. k2. n1 e n2 – Model Constants

Where  $C_0$  and  $k_0$  are the pre-exponential factors; T is the absolute temperature; R is the universal gas constant. 8.3145 J mol<sup>-1</sup> K<sup>-1</sup>;  $\Delta$ Hm (J mol<sup>-1</sup>). or the water absorption heat, is equal to the difference between the monolayer sorption heat (Hm) and the multilayer water sorption heat (Hn).  $\Delta$ Htc (J mol<sup>-1</sup>) is the difference between the latent heat of pure water vaporization (HG) and the sorption heat of multi-layer water (Hn).

To determine the parameters of the GAB equation, two methods were used. Direct regression is the method where Equations (4) and (5) are added to Equation (1), so all six parameters are determined together. In the indirect method, we determine the three parameters of the GAB equation individually for each temperature and then use a linearization of both Arrhenius (4) and (5) equations to determine the remainder of the parameters.

The criteria used to determine the best fit of the models to the experimental data was: the coefficient of determination ( $R^2$ ). the sum of the squares regression (SSE) and the absolute mean minimum percentage of error (P). calculated by Eq. 10.

$$R^2 = \frac{SSEr}{SSEt} \tag{7}$$

$$SSEr = \sum_{i=1}^{n} (Xeq(\exp) - Xeq(teo))^2$$
(8)

$$RMSE = \sqrt{\frac{SSE}{n-m}}$$
(9)

$$P = \frac{100}{n} \sum_{i=1}^{n} \left( \frac{X_{eq(exp)} - X_{eq(teo)}}{X_{eq(exp)}} \right)$$
(10)

Where,

- P-mean percentage deviation. %;
- X<sub>eq(exp)</sub> experimental equilibrium humidity. % d.b;

 $X_{eq(teo)}$  – equilibrium humidity estimated by the model. % d.b; e.

- n number of experimental data.
- m number of adjusted coefficients.

#### 2.6 Thermodynamic Properties

The isosteric sorption heat  $(Q_{st})$  was calculated according to the Clausius-Clapeyron equation (Eq. 11). Application of this method requires the determination of adsorption isotherms at least



three temperatures (Miltal & Usborne, 1985).

$$\partial \ln a w / \partial T = Qst / RT^2$$
 (11)

Where R is the gas constant (R = 8.314 J / mol / K). T is the absolute temperature (K) and Q<sub>st</sub> is the net isosteric adsorption heat (kJ mol<sup>-1</sup>). Integrating Eq. 12, we have the following relation:

$$\ln aw = \frac{\left(\frac{Qst}{R}\right)}{T} + K \tag{12}$$

To describe the relationship between equilibrium water content and Qst, the Reidel equation (Eq. 13) was used:

$$Qst = Cr e^{-BrXeq}$$
(13)

where Cr and Br are coefficients of the model.

The proposed calculation for thermodynamic properties was based on the Gibbs - Helmholtz energy calculated by Eq. 14:

$$\Delta G = RT \ln aw \tag{14}$$

Obtaining Gibbs free energy, differential entropy ( $\Delta$ S) was calculated from Eq. 15, this property is associated with the forces of attraction or repulsion between water molecules and product components and is linked to the spatial arrangement of the absorber, of water (Aksil et al., 2019).

$$\Delta S = \frac{\Delta H - \Delta G}{T} = (Qst - \Delta G)/T$$
(15)

Correlating the values obtained from  $\Delta H$  versus  $\Delta S$  for adsorption data, it is expected that a linear trend confirms the compensation theory for adsorption using Eq. 16. In this relationship. Tb is the isokinetic temperature and represents the temperature at which all reactions series are processed at the same speed.

$$\Delta H = Tb (\Delta S) + \Delta G \tag{16}$$

#### **3. Results and Discussion**

#### 3.1 Centesimal Composition of Fresh and Powdered Kernels

The proximate composition of kernel was chemically determined before and after the drying process, allowing the evaluation of changes in flour composition. Considering the data presented in Table 2, the moisture content presented a high value in fresh kernel, however after the drying process there was a reduction of approximately 95% in the amount of water



on the flour. This fact corroborates the studies of (Campidelli et al., 2019; Lisboa et al., 2019) confirming the need for the drying process to remove water from the product, providing safe storage. The increase on all other constituents is due to water removal. Analysing the contents of juá flour it is noticeable the greater amount of proteins, then fat and finally the carbohydrates.

Parameter	Kernel in natura	Kernel flour
Moisture (%)	$60.51 \pm 0.99$	$3.30\pm0.00$
Proteins (%)	$23.62 \pm 0.42$	$42.91\pm0.42$
Fats (%)	$7.64\pm0.25$	$25.98 \pm 0.50$
Ashes (%)	$1.79\pm0.13$	$4.35\pm0.02$
Carbohydrates (%)	$6.43\pm0.05$	$23.46\pm0.25$

Table 2. Centesimal composition of fresh and dried Ziziphus joazeiro kernel

#### 3.2 Adsorption Isotherms

Figure 1 shows the water adsorption isotherms of the kernel flour at temperatures of 293, 303 and 313 K, with adjustments by the GAB model. The equilibrium water content (Xeq, % b.s.) and water activity (a<sub>w</sub>) values were obtained in the range 2.070 to 33.08 and 0.1210 to 0.934, respectively. As expected, isotherms presented an increase in equilibrium water content with the increase in water activity. Also, for the same water activity, an higher equilibrium water content is found when the temperature is increased. This tendency suggests a reduction in the total number of active water binding sites. Particulary, as the temperature increases, the water molecules become more excited, thus reducing intermolecular interactions and decreasing the attraction force with the product material (Saleh, Karim, Hensel & Sturm, 2018; Santos et al., 2011).



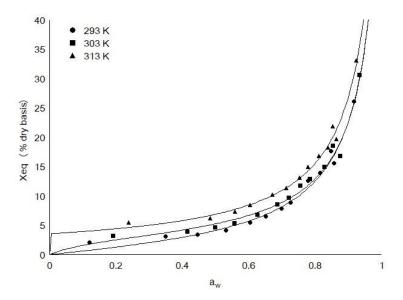


Figure 1. Water adsorption isotherms of juá kernel flour at 293, 303 and 313 K adjusted by the GAB model

From figure 1, all isotherm curves have a sigmoidal curve with an intermediate flat region thus reflecting the characteristics of type II isotherms. This type of isotherm can be classified into three regions: the first corresponds to the moisture of the monolayer strongly linked to the product matrix; the second is almost linear, corresponding to the water at the material multilayer; and the third region is related to the free water available for chemical reactions (Polachini et al., 2016; Torres & Seijo, 2016). Analysing figure 1, the first region occupies most of the isotherm, evidenced by the small increase in equilibrium moisture until water activities of 0.6. Since our flour is majorly composed by proteins and polysaccharides, this result suggests water is highly bound to these hydrophilic macromolecules (Chisté et al., 2015).

#### 3.3 Mathematical Modeling of the Absorption Isotherms

Water adsorption isotherms were determined for the juá kernel flour at temperatures of 293, 303 and 313 K. Table 3 presents the coeficients of the GAB model, determined by the direct and indirect method, and the Oswin and Peleg models. All models showed good fit to experimental data with values  $R^2$ > 0.98 and P <10%. The GAB model presented the best fits for temperatures of 303 and 313 K with  $R^2 = 0.99$  and P <6%. The Peleg model presented the best adjustment for the temperature of 20°C with  $R^2 = 0.99$  and P <6%. The GAB model determined by the indirect regression presented the best adjustments for the studied temperatures for the juá kernel flour.

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Table 3. Regressed parameters of the GAB, Peleg and Oswin models of the juá kernel flour adsorption isotherm, coefficients of determination (R<sup>2</sup>) and mean percentage deviations (P) at temperatures of 293, 303 and 313 K

$\frac{Xm}{3.45 \pm 0.004}$	С	k	ΔHm						
3 45 + 0 004			ΔHm	∆Htc					
$3.45 \pm 0.004$			-18497.4	2501.41					
5.45 ± 0.004	$3.82\pm0.005$	$0.95\pm0.001$			98.34	14.73	0.67	12.6	Random
$4.44 \pm 0.002$	$4.57\pm0.007$	$0.92\pm0.002$			99.39	12.68	0.62	9.48	Random
$5.62 \pm 0.008$	$5.42 \pm 0.004$	$0.90 \pm 0.008$			98.73	9.45	0.54	6.12	Random
Xm	С	k	ΔHm	ΔHtc	R <sup>2</sup> (%)	SSE	RMSE	P(%)	Residual versus predicted
			-130172.3	-409.382					•
$5.00 \pm 0.004$	$1.48\pm0.002$	$0.91\pm0.003$			99.51	21.96	0.82	10.8	Random
$4.66 \pm 0.006$	$7.40\pm0.003$	$0.92\pm0.001$			99.29	38.46	1.08	10.6	Random
$4.56 \pm 0.006$	$45.60 \pm 0.008$	$0.93 \pm 0.006$			99.55	10.96	0.58	5.6	Random
Coefficients			R <sup>2</sup> (%)	SSE	RMSE	P(%)		Residual versus predicted	
k1	nl	k2	n2						
35.3 ± 0.015	$5.00\pm0.01$	$5.35\pm0.20$	$0.48\pm0.01$	98.73	9.45	0.54	12.6		Random
$33.7\pm0.50$	$5.14\pm0.02$	$4.33\pm0.01$	$0.36\pm0.01$	98.97	7.62	0.49	5.73		Random
									Random
;	a	b	1	R <sup>2</sup>	SSE	RMSE	P(%)		Residual versus predicted
5.80 ±	0.001	0.70 ±	0.01	98.25	12.98	0.63	13.54		Random
303 K 6.76 ± 0.002		0.55 0.000		00.10	5 70	0.42	0.2		
6./6 ±	0.002	0.57 ±	0.008	99.18	5.79	0.42	8.3		Random
8,30 -	+ 0.01	0.54 +	- 0.02	99.00	6.24	0.44	6.55		Biased
5 5 4 4 3 3	$5.62 \pm 0.008$ $Xm$ $5.00 \pm 0.004$ $4.66 \pm 0.006$ $4.56 \pm 0.006$ $k1$ $35.3 \pm 0.015$ $33.7 \pm 0.50$ $35.20 \pm 0.01$ $5.80 \pm 6.76 \pm 0.001$	$5.62 \pm 0.008  5.42 \pm 0.004$ $Xm  C$ $5.00 \pm 0.004  1.48 \pm 0.002$ $4.66 \pm 0.006  7.40 \pm 0.003$ $4.56 \pm 0.006  45.60 \pm 0.008$ $Coeffick1  n1$ $35.3 \pm 0.015  5.00 \pm 0.01$ $33.7 \pm 0.50  5.14 \pm 0.02$	$5.62 \pm 0.008  5.42 \pm 0.004  0.90 \pm 0.008$ $\hline Xm  C  k$ $5.00 \pm 0.004  1.48 \pm 0.002  0.91 \pm 0.003$ $4.66 \pm 0.006  7.40 \pm 0.003  0.92 \pm 0.001$ $4.56 \pm 0.006  45.60 \pm 0.008  0.93 \pm 0.006$ $\hline Coefficients \\ \hline k1  n1  k2 \\ 35.3 \pm 0.015  5.00 \pm 0.01  5.35 \pm 0.20 \\ 33.7 \pm 0.50  5.14 \pm 0.02  4.33 \pm 0.01 \\ \hline 35.20 \pm 0.01  6.00 \pm 0.002  9.30 \pm 0.30 \\ \hline a \qquad b \\ \hline 5.80 \pm 0.001 \qquad 0.70 \pm 0.01 \\ 6.76 \pm 0.002 \qquad 0.57 \pm 0.002 \\ \hline 0.57 \pm 0.001 \\ \hline 0.008  0.001  0.001  0.001 \\ \hline 0.001  0.001  0.001  0.001 \\ \hline 0.001  0.001  0.001  0.001 \\ \hline 0.001 $	Xm       C       k $\Delta Hm$ -130172.3         5.00 ± 0.004       1.48 ± 0.002       0.91 ± 0.003         4.66 ± 0.006       7.40 ± 0.003       0.92 ± 0.001         4.56 ± 0.006       45.60 ± 0.008       0.93 ± 0.006         Coefficients         k1       n1       k2       n2         35.3 ± 0.015       5.00 ± 0.01       5.35 ± 0.20       0.48 ± 0.01         33.7 ± 0.50       5.14 ± 0.02       4.33 ± 0.01       0.36 ± 0.01         a       b       5.80 ± 0.001       0.70 ± 0.01         6.76 ± 0.002       0.57 ± 0.008       0.57 ± 0.008	Xm       C       k $\Delta Hm$ $\Delta Hc$ -130172.3       -409.382         5.00 $\pm$ 0.004       1.48 $\pm$ 0.002       0.91 $\pm$ 0.003         4.66 $\pm$ 0.006       7.40 $\pm$ 0.003       0.92 $\pm$ 0.001         4.56 $\pm$ 0.006       45.60 $\pm$ 0.008       0.93 $\pm$ 0.006         Coefficients       R <sup>2</sup> (%)         k1       n1       k2       n2         35.3 $\pm$ 0.015       5.00 $\pm$ 0.01       5.35 $\pm$ 0.20       0.48 $\pm$ 0.01       98.73         33.7 $\pm$ 0.50       5.14 $\pm$ 0.02       4.33 $\pm$ 0.01       0.36 $\pm$ 0.01       99.62         a       b       R <sup>2</sup> 5.80 $\pm$ 0.001       0.70 $\pm$ 0.01       98.25         6.76 $\pm$ 0.002       0.57 $\pm$ 0.008       99.18	$x_m$ C       k $\Delta Hm$ $\Delta Htc$ $R^2$ (%)         -130172.3       -409.382       -130172.3       -409.382         5.00 $\pm$ 0.004       1.48 $\pm$ 0.002       0.91 $\pm$ 0.003       99.51         4.66 $\pm$ 0.006       7.40 $\pm$ 0.003       0.92 $\pm$ 0.001       99.29         4.56 $\pm$ 0.006       45.60 $\pm$ 0.008       0.93 $\pm$ 0.006       99.55         Coefficients       R <sup>2</sup> (%)       SSE         k1       n1       k2       n2         35.3 $\pm$ 0.015       5.00 $\pm$ 0.01       5.35 $\pm$ 0.20       0.48 $\pm$ 0.01       98.73       9.45         33.7 $\pm$ 0.50       5.14 $\pm$ 0.02       4.33 $\pm$ 0.01       0.36 $\pm$ 0.01       99.62       2.37         a       b       R <sup>2</sup> SSE       5.80 $\pm$ 0.001       0.70 $\pm$ 0.01       98.25       12.98         5.80 $\pm$ 0.001       0.70 $\pm$ 0.01       98.25       12.98       5.79	$x_{m}$ C       k $\Delta Hm$ $\Delta Hc$ $R^{2}$ (%)       SSE $x_{m}$ C       k $\Delta Hm$ $\Delta Hc$ $R^{2}$ (%)       SSE $x_{0}$ 0.004       1.48 ± 0.002       0.91 ± 0.003       -130172.3       -409.382 $x_{0}$ $x_{0}$ $x_{0}$ $x_{0}$ $x_{0}$ $y_{0}$ $y_{0}$ $x_{0}$ $x_{0}$ $x_{0}$ $x_{0}$ $y_{0}$ $y_{0}$ $y_{0}$ $y_{0}$ $x_{0}$ $x_{0}$ $x_{0}$ $x_{0}$ $y_{0}$ $y_{$	$x_m$ C       k $\Delta Hm$ $\Delta Hc$ $R^2$ (%)       SSE       RMSE $x_m$ C       k $\Delta Hm$ $\Delta Hc$ $R^2$ (%)       SSE       RMSE $-130172.3$ $-409.382$ $-130172.3$ $-409.382$ $99.51$ $21.96$ $0.82$ $5.00 \pm 0.004$ $1.48 \pm 0.002$ $0.91 \pm 0.003$ $99.29$ $38.46$ $1.08$ $4.66 \pm 0.006$ $7.40 \pm 0.003$ $0.92 \pm 0.001$ $99.29$ $38.46$ $1.08$ $4.56 \pm 0.006$ $45.60 \pm 0.008$ $0.93 \pm 0.006$ $99.55$ $10.96$ $0.58$ Coefficients       R <sup>2</sup> (%)       SSE       RMSE       P (%)         k1       n1       k2       n2 $-130172.3$ $9.45$ $0.54$ $12.6$ $33.7 \pm 0.50$ $5.14 \pm 0.02$ $4.33 \pm 0.20$ $0.48 \pm 0.01$ $98.97$ $7.62$ $0.49$ $5.73$ $35.20 \pm 0.01$ $6.00 \pm 0.002$ $9.30 \pm 0.30$ $0.33 \pm 0.01$ $99.62$ $2.37$ $0.26$ $3.4$ a       b       R <sup>2</sup> SSE       RMSE       P (%) $5.80 \pm 0.001$ $0.70 \pm 0.01$ <td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Molecular monolayer  $(X_m)$  is a critical parameter as it represents the water content at which the rate of any associated reaction will be negligible due to the strong water binding to the product matrix (Yogendrarajah et al., 2015). Considering the best model, the values of Xm, decreased with increasing isotherm temperature, from 5.0% to 4.56%. From a practical point of view this means that drying below this value tends to produce a high energy expenditure due to the strong water binding (Torres & Seijo, 2016). The water activity values for each Xm value were 0.566, 0.543 and 0.275 for temperatures of 293, 303 and 313 K, respectively, and are considered optimal values for product stability during storage as pointed by (Aksil et al., 2019).

Parameter C is related to potential chemical differences between the monolayer and the upper layer (Santos et al., 2011). The values of this parameter ranged from 1.26 to 45.61 and followed an upward trend with temperature. This trend is probably due to the strong binding energy of water molecules in the monolayer, and may also be related to a higher rate of surface evaporation due to greater excitation of water molecules (Baptestini et al., 2017).

The constant K of the GAB model represents the capacity of multi-layer water adsorption (Abebe & Ronda, 2015). K values of juá flours presented values ranging between 0.91 and 0.93. It is common to find higher K values in drier products. which confirms the trend reported by (Polachini et al., 2016), which observed increasing values of K as the temperature gets higher and, consequently, the equilibrium moisture content and the monolayer humidity

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decrease. Higher K values indicate that the multilayer sorption heat is higher at higher temperatures, which means that the monolayer sorption heat tends to be higher than the multilayer (Santos et al., 2011).

Analyzing the parameters of C and K of the GAB model, the water adsorption isotherms for juá flour are Type II (sigmoid form), according to the classification of (Blahovec, 2004) because they presented  $0 < K \le 1$  and C > 2.

# 3.4 Thermodynamic Properties

Figure 2 presents the isosteric heat ( $Q_{st}$ ) as a function of equilibrium water content ( $X_{eq}$ ). It was observed that  $Q_{st}$  decreases with increasing equilibrium moisture ranging between 4336.3 and 194.8 k J / mol. This indicates that high Qst values are found at lower moisture contents. This behavior corroborates the results of (Aksil et al., 2019; Polachini et al., 2016; and Nascimento et al., 2019). The results indicate that there is a strong bond between the water molecules and the molecules present in the product monolayer, however, a rapid decrease in isosteric heat of adsorption occurs when the moisture content begins to increase due to the adsorption of water molecules in the multilayer. Also, according to (Freitas et al., 2016 and Nascimento et al., 2019) greater energy is required to remove water from dry products. Moreover, Reidel equation was used to fit the the experimental data by non-linear regression. The regression coefficients were Cr = 10153.2 J / mol and Br = 0.295 and the coefficient of determination was R<sup>2</sup> = 0.85.

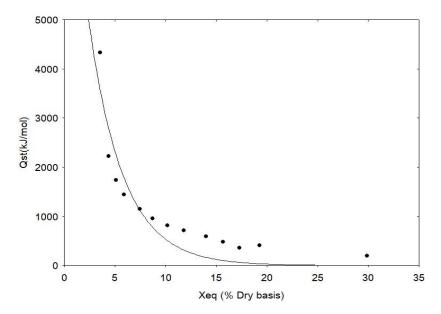


Figure 2. Isosteric heat (Qst) as a function of equilibrium moisture content (Xeq)

The relation between enthalpy ( $\Delta$ H) and entropy ( $\Delta$ S) is defined as the compensation theory, which is an important point to demonstrate the dependence of these thermodynamic parameters on equilibrium water content. A linear trend is observed in Figure 3, with R<sup>2</sup>> 0.999, indicating simultaneous changes in enthalpy, entropy and Gibbs free energy. According to (Polachini et al., 2016), the enthalpy that is associated with Gibbs free energy tends to assume values close to zero when the equilibrium water content is increased,



indicating that the process is spontaneous when there is multilayer adsorption of water molecules.

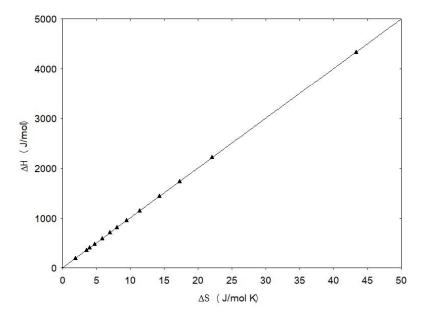


Figure 3. Enthalpy ( $\Delta$ H) -entropy ( $\Delta$ S) ratio of adsorption processes for juá kernel flour

From the graph shown in Figure 4, a value of 373.15 K was obtained for the isokinetic temperature, which is defined as the temperature at which all reactions occur. The presence of higher T<sub>b</sub> values (above 300 K) were characteristics observed and reported by (Polachini et al., 2016) for products with high sugar or starch content, such as potato, plum and apricot.

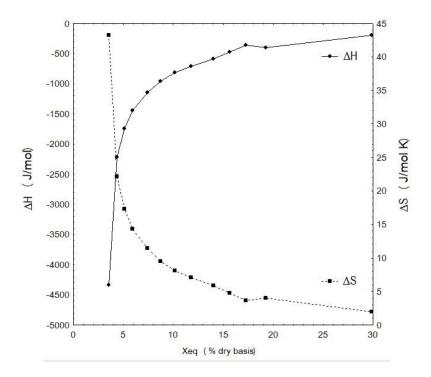


Figure 4. Influence of equilibrium moisture content on enthalpy and entropy change



Figure 4 shows the differential behavior of enthalpy and entropy associated with the adsorption process, providing information about the reaction in the water / structure system. It is observed that the moisture content directly influences the increase of entropy and the decrease of enthalpy, decreasing the energy necessary to perform a useful work. In theory (Castro-Muñoz, 2018) have shown that increasing water content provides these entropy and enthalpy values due to the structural transformation of solubilization and swelling that allows for greater mobility of adsorbed molecules.

# 4. Conclusions

The present study demonstrated that the adsorption isotherms of juá kernel flour (*Ziziphus joazeiro*) at temperatures of 293, 303 and 313 K presented typical type II adsorption behavior, with values of  $0 < K \le 1$  and C > 2. In water activities below 0.6 there was a linear increase in equilibrium water content, and above this value this growth was exponential at all temperatures studied. With in the temperature range investigated the GAB model presented the best correlation with the experimental data. The liquid isosteric heat of sorption decreased exponentially with increasing moisture content. Compensation theory demonstrates the dependence between entropy ( $\Delta$ S), enthalpy ( $\Delta$ H) and equilibrium water content, configuring in a spontaneous and typically enthalpy process. The study provides unprecedented and essential information for the understanding of hygroscopic and thermodynamic parameters, facilitating the subsequent applications of this product, aiming at better storage.

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